

**NEW APPROACHES TO THE IMPLEMENTATION OF THE MINING TECHNOLOGY OF DIMENSION STONE USING A CLOSE-SET DRILLING**

*The analysis of the current state the non-blasting monolith extraction technology was conducted. The further research direction was substantiated. Has been considered and justified the rational parameters of close-set drilling technology of dimension stones. Solution is offered that consist the combined drilling (a close-set and a holes line drilling), that provides to increase of stone splitting efficiency under its own weight. The calculation of the parameters of the scheme of partial underdrilling at a monolith of stone with the purpose of reducing the volume of drilling works is given. Diagrams of tensile stress changes depending on the specific area of splitting were built. A rational correlation between the drilling parameters of the holes has been established by solving the problems of loading the cantilever beam and stress concentration by the Kirsch solution. The most important parameter for the implementation of this technology is the ratio of monolith height to its length. Engineering formulas are proposed for calculating the technological parameters of the realization of the "gravitational-hole" stone splitting. The configuration of a rough block of stones is determined under which this technology can be realized. Creating of close-set holes provides the increase of maximal tensile stress with equal values of specific splitting area ratio. It is established that the effective drilling depth of close-set holes is 43,2 % of monolith height. It is estimated that combined drilling method application of savings from drilling operation will be 11,36 %.*

**Keywords:** *dimension stone; non-explosive of mining processes; drilling of boreholes; brittle fracture.*

Introduction and problem statement. The technology of mining dimension stone intended to perform separation of regular geometric shape of stone parts while preserving its properties of strength and integrity. These criteria corresponds to a number of nonexplosive mining technologies where the basic principle of material failure is to create separation cracks due to the abrasive cutting and drilling. The Abrasive cutting is performed by diamond wire saws and their use may be limited by the presence of a well-developed rock jointing, with a high probability of clamping diamond rope. Another technology is a technology close-set stone drilling aimed at creation of cracks by drilling a line of holes. The quality properties of stone extracted in this way can be compared only with the diamond wire cutting technology. With maximum preservation of the stone, this technology is not without drawbacks, such as the loss of stone during the gaping formation, the width of which is equal to the diameter of the hole. In addition, the close-set drilling technology is characterized by large volumes of drilling, which is quite costly. This technology is the only possible in difficult geological conditions and mining of large-sized monoliths. It is possible to overcome its main drawback ( the large volume of drilling operations) through the development of technology for splitting of the monolith under its own weight with a partial close-set drilling. It requires a detailed study and an analysis of rock splitting power parameters and the connection to geometric parameters of mining processes.

Analysis of researches and publications. The technology of close-set drilling is the simplest of all splitting technologies as the main research of it was to evaluate the volume of stone losses. This issue is dedicated to the works of such scholars as O. O. Kisel , V.V. Kotenko, and V.V. Korobyichuk [1-5]. The Basic research is the geometric patterns calculations of the stone loss during the close-set drilling of monoliths and solution are reduced to the study options that would ensure minimal production losses. Another weak point of this technology is the accuracy of the drilling operation of a continuous line of the holes depending on volume of stone losses. This issue was thoroughly studied by R. V. Sobolewskiy, and A. V. Shlapak [6]. Major decisions and recommendations for this technology are to determine the limits of deviation from the vertical axis of the holes without significant loss of stone volume. In scientific literature the questions of physics processes in the large monoliths extraction were considered by such scientists as M. T. Bakka , S. A. Zhukov, K. K. Tkachuk. They investigated the power settings ensuring splitting of large size stone monoliths [7-9, 12–20]. The splitting methods considered in their works did not provide such preservation and quality, as a method of close-set holes drilling. It is first time, when the possibility of splitting stone using the forces caused by the stone own weight was considered [10, 11]. In theory it was proved that the possibility of splitting during previous horizontal drilling of holes line, that should ensure the monolith position in the array as a cantilevered beam and further splitting in the plane creating the largest tensile stress. However, in the application to real parameters of monoliths separation this possibility has not been studied in detail. This technology requires a detailed study and analysis to establish rational boundaries of drilling technological parameters and maximum savings.

The aim of the articles is to determine technological parameters of line holes drilling during the of the monolith stone separating process using gravity-hole splitting.

Basic material report of the article.

The technology of the close-set monolith drilling is realized by drilling hole line of increased diameter with a certain level of overlap that except the formation of an abutment between them. Reducing the cost of this technology can be achieved by drilling holes in a solid line on a certain depth and drilling in holes on the entire height of the specified interval (Fig. 1).

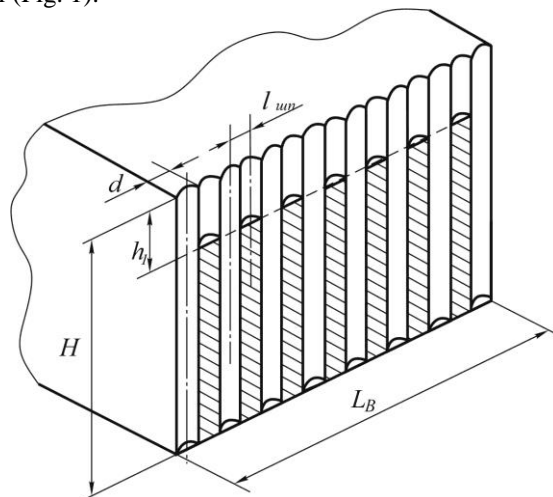


Fig. 1. Drilling scheme in the implementation of stone splitting by the gravitational method

With this method of extraction the splitting in the abutment between the holes will be provided by the effort made by the monolith's own weight. With the implementation of this technology the basic calculation will be to establish the value of the area to begin the activation of splitting rocks of specified weight depending on the geometrical parameters of the monolith. In general the formula determining this dependence is described by equations to determine the stress of a cantilever beam taking into account stress concentration on the walls of holes while finding the solution to the Kirsch's problem [10,11]:

$$\sigma_{\min} = \frac{9\rho g l^2}{K_s \cdot b \cdot h^2}, \quad (1)$$

where  $\rho$  – the density rocks of the monolith,  $t/m^3$ ;  $l$  – the length of the monolith (distance from the splitting line to the free surface of open-pit bench), m;  $K_s$  - ratio of the specific splitting plane (the ratio of the area of line holes to the total area of the monolith splitting);  $b$  - width of the monolith, m;  $h$  - the height of the monolith, m.

As practice shows extraction of crystalline rocks, the average value of the limit of tensile strength at which the gradual stone destruction varies from 8 MPa to 12÷15 MPa (passports strength). In the calculations of the entire height of the monolith drilling according to formula 1 and the given parameter, the process of steady stone splitting begins when the ratio of the splitting specific plane is about 4,5%. In this case, it is necessary to split almost the entire area and to perform drilling operations in the amount of 95,5 % from the amount of work in the close-set drilling. Implementing this, the technology of gravity-hole stone splitting is quite inefficient and a slight decrease in drilling volume is observed only in comparison with the line of drilling holes. The drilling volumes may be decreased slightly by running the process of close-set drilling holes only at the top of the monolith.

The formula 1 shows that increasing the ratio of monolith length  $l$  to height  $h$  separating area will increase the volume of splitting forces, and consequently to reduce the required volume of drilling operations. From the technological point of view there is no possibility to change the ratio of the length of the monolith to its height, so the only way this value varies due to the close-set drilling of the top layer of the marked splitting area (Fig. 2). In addition, the weight of the layer located above the line of maximum tensile with the magnitude of this layer  $h_1$  causes the increase of the stress.

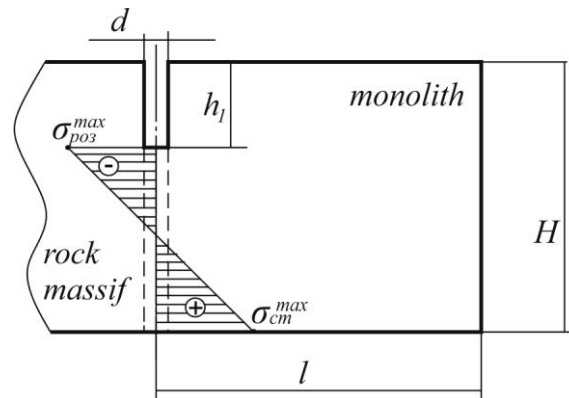


Fig. 2. The diagram of the forces in the stone splitting by the gravitational method

Taking into account the close-set drilling of the monolith upper layer and the weakening the splitting area of the lower layer by drilling line of holes with some interval the formula for calculating the maximum tensile stress will be as follows (2):

$$\sigma_{\max} = \frac{9\rho g \left(1 + \frac{h_1}{H}\right) l^2}{K_s \cdot b \cdot (H - h_1)^2} \quad (2)$$

The calculation was performed for the parameters of the monolith length  $l = 6$  m; height of the monolith  $h = 5$  m and density of the rock mass  $2,85 \text{ t/m}^3$ . The range of the ratio value of the specific splitting plane is  $0,011 \div 1,0$ . The diagrams of maximum stresses changes were built according to the analytical expression of the formula 2 and the initial conditions expressed by the ratio of the specific plane of splitting (Fig. 3). It is necessary to consider also that the maximum ratio value of the specific splitting planes corresponds to the ratio of drilling-hole diameter to the distance between holes  $K_s = d_{\text{mm}}/l_{\text{mm}}$ , with known diameter value of 40 mm and the allowed distance between holes of 200 mm, providing high-quality of stone splitting, the maximum value of  $K_s$  will be 0,2.

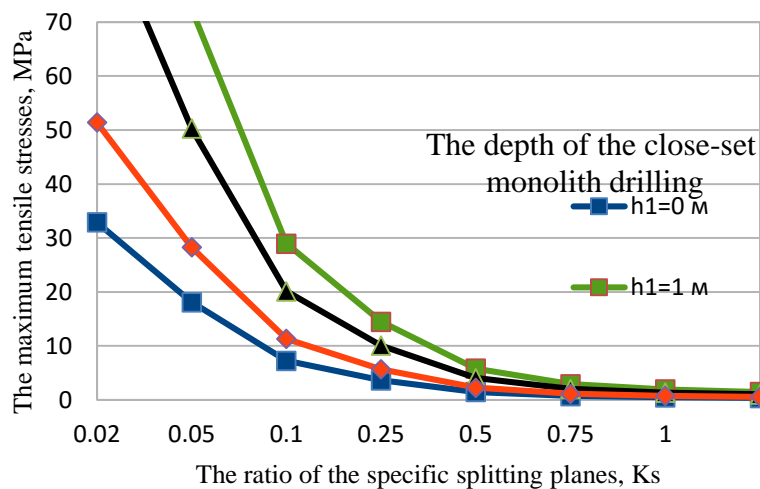


Fig. 3. Diagrams of tensile stress changes depending on the specific area of splitting

The diagrams in figure 3 shows the creation of a pre-drilled line of holes providing an increase in the maximum tension stress with equal ratio values of the specific splitting planes. Thus the close-set drilling makes the desired effect and at the maximum value of  $K_s=0,2$  the depth of drilling the line of holes will be 2,16 m or 43,2 % of the monolith height. The drilling volume of this splitting plane are defined as the amount of the close-set drilled plane and the amount of exposure areas formed by line of holes, that is 88,64 % of the total splitting area. In this case the amount of savings from drilling in comparison with the technology of a close-set drilling are 11,36 %, that is 2,5 times better economy indicator of drilling than in the previous case.

Conclusions. According to the analytical investigations and calculations, the efficiency of the technologies of gravity-hole stone extraction was established using the proposed drilling scheme and calculation formula. The maximum value of the effective depth of close-set drilling holes line is 43,2 % of the total drilling depth. The maximum amount of savings from drilling applying this method will be 11,36 %. This technology is effective in extracting of large size blocks of stone, where the main condition is the preservation of its integrity.

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